



**UTM**  
UNIVERSITI TEKNOLOGI MALAYSIA

OPENCOURSEWARE

# Thermodynamics I

## Chapter 4

### First Law of Thermodynamics

### Open Systems

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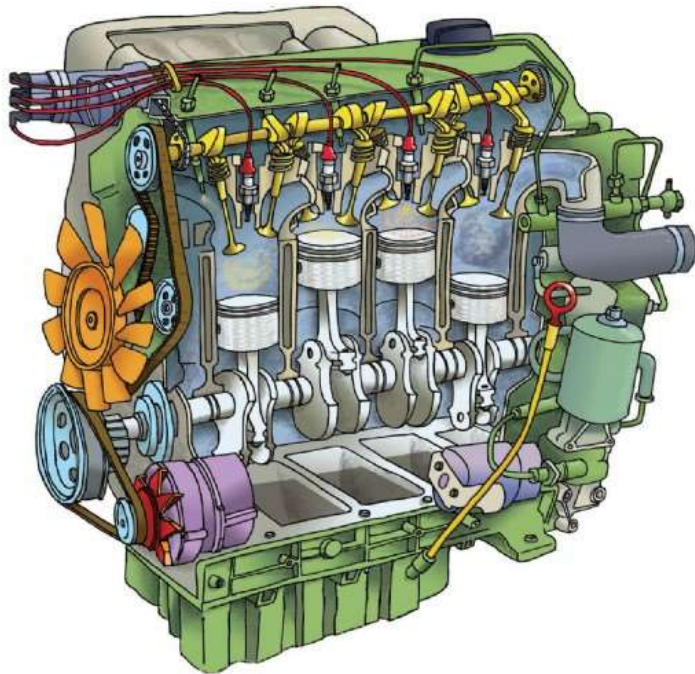
# First Law of Thermodynamics (Motivation)

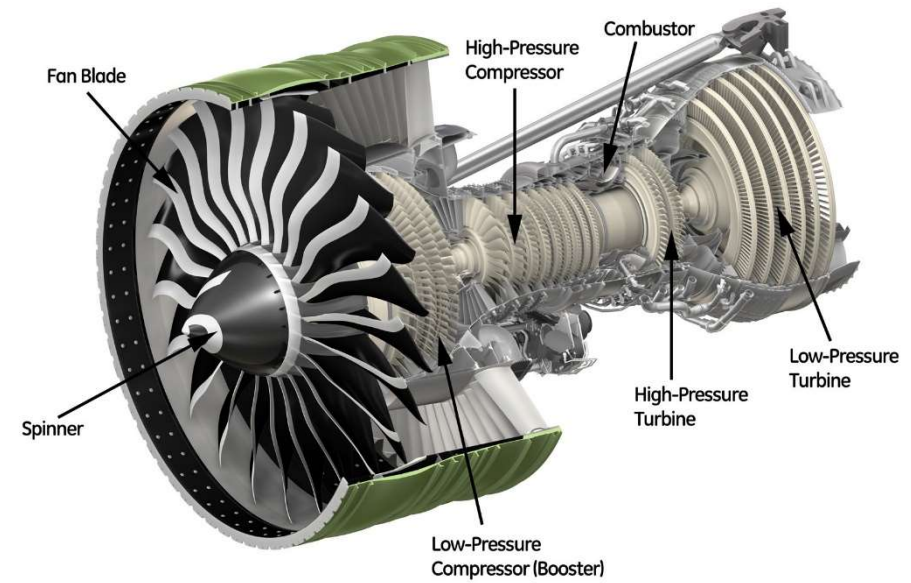
A system changes due to interaction with its surroundings.

Interaction study is possible due to conservation laws.

Various forms of conservation laws are studied in this chapter in the form of balance equations.

# Examples of Open Systems







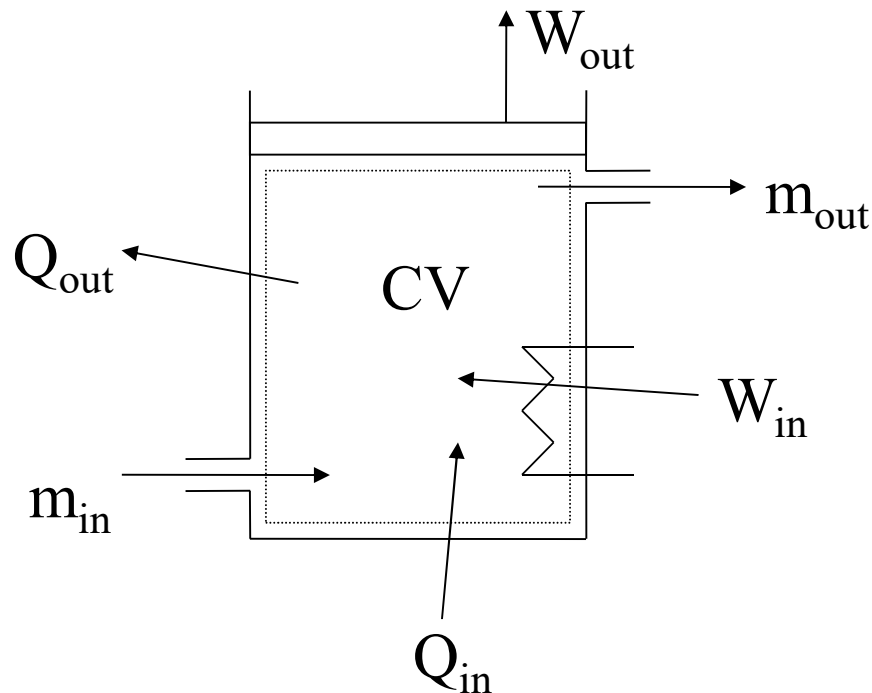


## 1ST LAW FOR OPEN SYSTEMS

Energy and Mass can enter/leave an open system

Divided into two parts:

- Conservation of Mass Principle
- Conservation of Energy Principle



# Mass Conservation (Mass Balance)

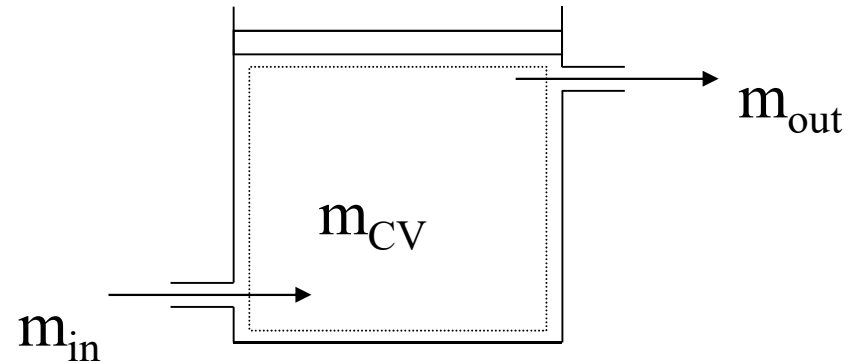
## Mass Balance:

$$\Delta m_{CV} = \sum m_{in} - \sum m_{out}$$

Net change  
of mass of  
CV

Total of all  
mass entering

Total of all  
mass exiting



$$\frac{dm_{CV}}{dt} = \sum \frac{dm_{in}}{dt} - \sum \frac{dm_{out}}{dt}$$

Rate of  
change of  
mass of  
CV

Total of all mass  
flow rates for all  
inlet channels

Total of all mass  
flow rates for all  
exit channels

## Mass flow rates and Speed for a channel

$$m = \rho V$$

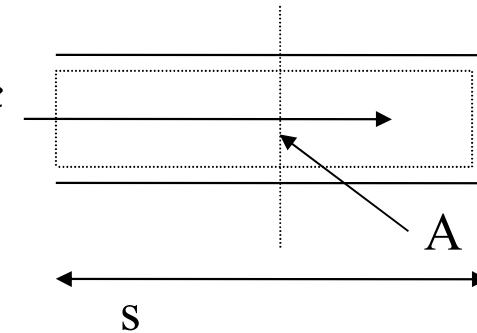
$$m = \rho s A$$

For flow rates;

$$\frac{dm}{dt} = \rho \frac{ds}{dt} A$$

$$\dot{m} = \rho \vec{V} A$$

$$\dot{m}, \rho, \vec{V}$$



but

$$sA = V$$

Thus;

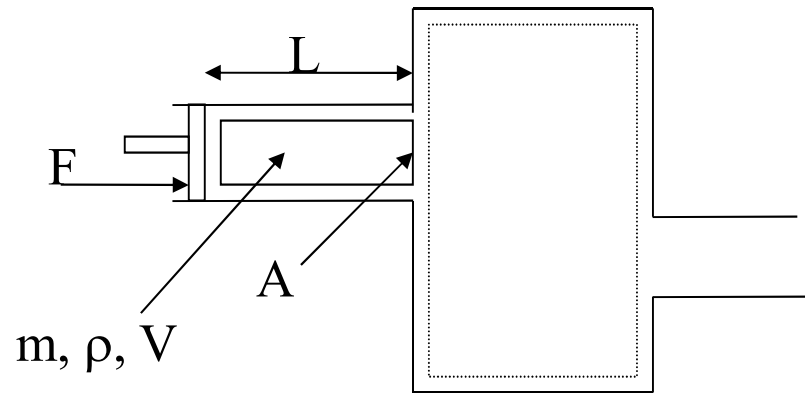
$$\dot{m} = \rho \vec{V} A = \frac{\vec{V} A}{v} = \rho \dot{V} = \frac{\dot{V}}{v}$$

$$\frac{ds}{dt} A = \dot{V}$$



## Flow Work

For an amount of mass to cross a boundary, it needs a force (work) to push it; called Flow Work ,  $w_{\text{flow}}$



The force that pushes the fluid;

$$F = PA$$

Work that is involved;

$$W = \int F \cdot ds$$

$$W_{\text{flow}} = F \cdot L$$

$$= PA \cdot L$$

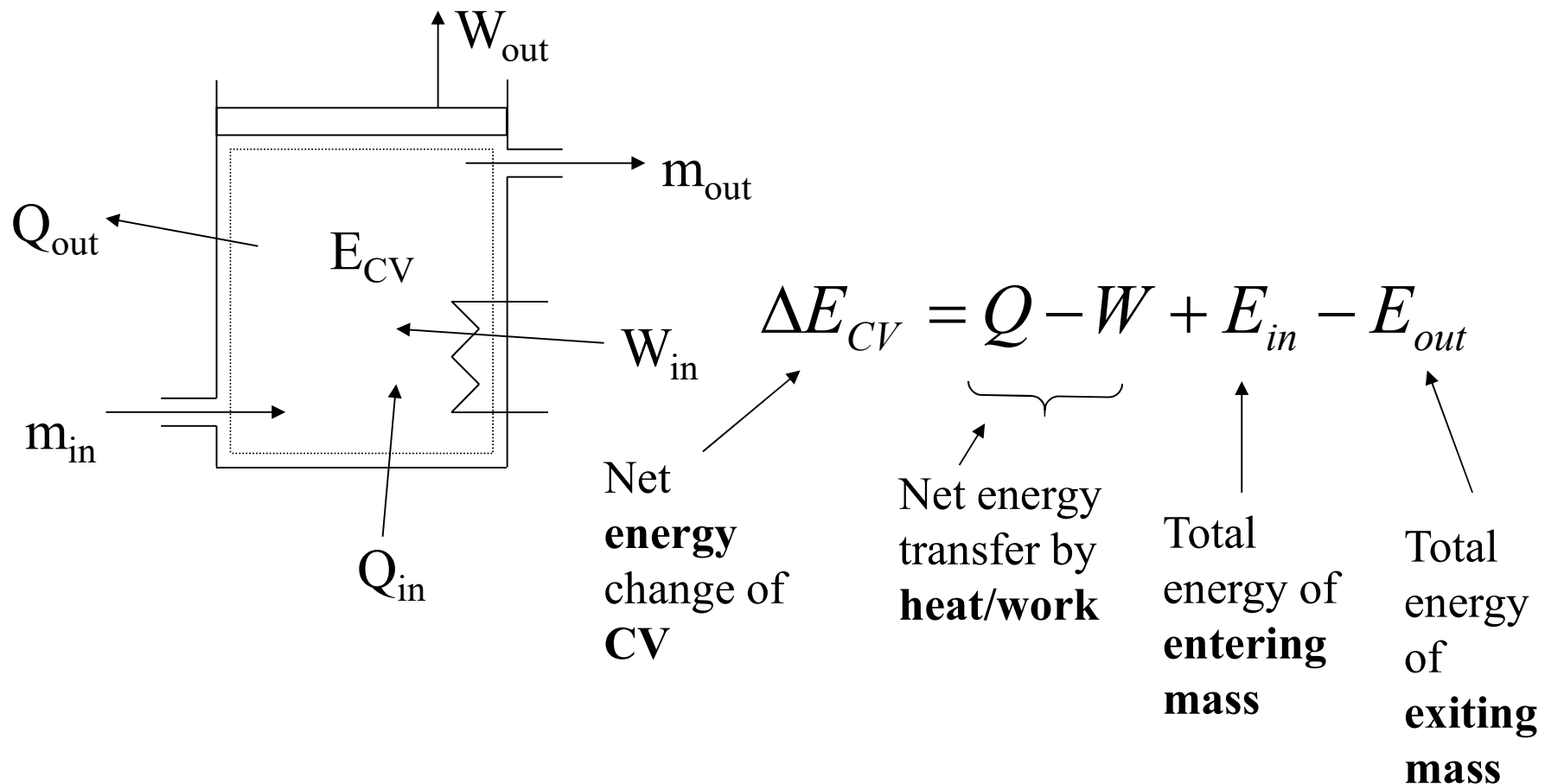
$$= PV$$

$$w_{\text{flow}} = pv$$

# Conservation of Energy for Open Systems

Energy can enter/leave an open system via

Heat, Work AND Mass Flow Entering/Leaving



## Energy of a Flowing Mass

An amount of mass possesses energy,  $E$ ,  $e$

$$e = u + ke + pe$$

but a flowing mass also possesses flow work, so

the Energy for a flowing mass;  $e_{\text{flow}}$

$$\begin{aligned} e_{\text{flow}} &= u + ke + pe + w_{\text{flow}} \\ &= u + pv + ke + pe \end{aligned}$$

but  $u + pv = h$  (enthalpy)

$e_{\text{flow}} = h + ke + pe$	(energy for a <u>flowing mass</u> )
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## Energy Balance for an Open System

can be written as;

$$\Delta E_{CV} = Q - W + E_{flow\,in} - E_{flow\,out}$$

or;

$$\Delta e_{CV} = q - w + e_{flow\,in} - e_{flow\,out}$$

$$= q - w + (h + ke + pe)_{in} - (h + ke + pe)_{out}$$

$$= q - w + \sum_{in} \underbrace{(h + ke + pe)}_{\text{For each inlet}} - \sum_{out} \underbrace{(h + ke + pe)}_{\text{For each outlet}}$$

Total of all work  
**except** flow work

For each  
inlet

For each  
outlet

but;

$$\Delta e_{CV} = (\Delta u + \Delta ke + \Delta pe)_{CV}$$

so;

$$(\Delta u + \Delta ke + \Delta pe)_{CV} = q - w$$
$$+ \sum_{in} (h + ke + pe) - \sum_{out} (h + ke + pe)$$

Energy Balance in other forms;

$$\Delta E_{CV} = Q - W + \sum_{in} (H + KE + PE) - \sum_{out} (H + KE + PE)$$

Rate form;

$$\frac{dE_{CV}}{dt} = \dot{Q} - \dot{W} + \sum_{in} \dot{m}(h + ke + pe) - \sum_{out} \dot{m}(h + ke + pe)$$

↑  
(general form of Energy Balance for an Open System)



## USUF, Transient Flow, Unsteady Flow

The general form of Energy Balance can also be used for the Uniform State, Uniform Flow system (*USUF*), or sometimes called *Transient Flow*.

*Charging* and *Discharging* cases of Transient Flow can be analyzed using the simplified form of the general energy balance below

$$\Delta E_{CV} = \dot{Q} - \dot{W} + \sum_{in} \dot{m}(h + ke + pe) - \sum_{out} \dot{m}(h + ke + pe)$$

$$\Delta U + \Delta KE + \Delta PE = \dot{Q} - \dot{W} + \sum_{in} \dot{m}(h + ke + pe) - \sum_{out} \dot{m}(h + ke + pe)$$

## Steady Flow Process

Criteria;

All *system properties* (intensive & extensive) do not change with time

$$m_{cv} = \text{constant}; \Delta m_{cv} = 0$$

$$V_{cv} = \text{constant}; \Delta V_{cv} = 0$$

$$E_{cv} = \text{constant}; \Delta E_{cv} = 0$$

Fluid properties at all *inlet/exit channels* do not change with time  
(Values might be different for different channels)

$$(\dot{m}, \vec{V}, A, \text{etc})$$

*Heat and work* interactions do not change with time

$$\dot{Q} = \text{constant}$$

$$\dot{W} = \text{constant}$$

## Implication of Criterion 1

**(Mass)**

$$\Delta m_{CV} = 0,$$

From Mass Conservation;

$$\sum \dot{m}_{in} - \sum \dot{m}_{out} = \Delta m_{CV}$$

$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$

Recall that

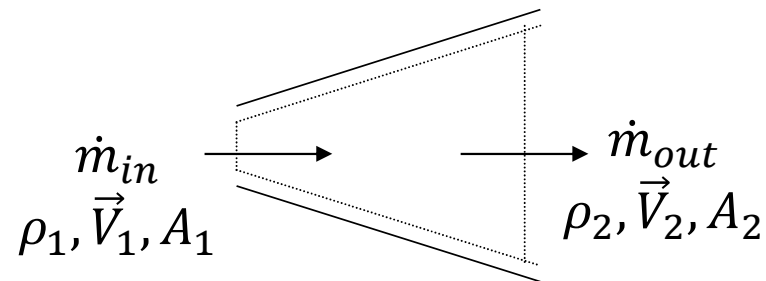
$$\dot{m} = \rho \vec{V} A = \frac{\vec{V} A}{v}$$

so

$$\sum_{i=1}^n \rho_i \vec{V}_i A_i \Big|_{in} = \sum_{o=1}^k \rho_o \vec{V}_o A_o \Big|_{out}$$

## Implication of Criterion 1 (**Mass**) ctd.

for 1 inlet/ 1 exit;



$$\dot{m}_{in} = \dot{m}_{out}$$

$$\rho_1 \vec{V}_1 A_1 = \rho_2 \vec{V}_2 A_2$$

## Implication of Criterion 1

**(Volume)**

$$\Delta V_{CV} = 0,$$

$$\therefore W_B = 0 (\text{boundary work} = 0)$$

$$\Delta E_{CV} = Q - W + \Sigma E_{\text{flow(in)}} - \Sigma E_{\text{flow(out)}}$$

$$W = W_{\text{electrical}} + W_{\text{shaft}} + \underset{0}{W_{\text{boundary}}} + \underset{\text{in h}}{W_{\text{flow}}} + W_{\text{etc.}}$$

W not necessarily 0, only  $W_B$  is 0

## Implication of Criterion 1

### (Energy)

$$\Delta E_{CV} = 0,$$

From Energy Conservation;

$$\frac{dE_{CV}}{dt} = \dot{Q} - \dot{W} + \sum_{in} \dot{m}(h + ke + pe) - \sum_{out} \dot{m}(h + ke + pe)$$

$\searrow$   
 $= 0$

Rearrange to get Steady State, Steady Flow Energy Equation

(SSSF)

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

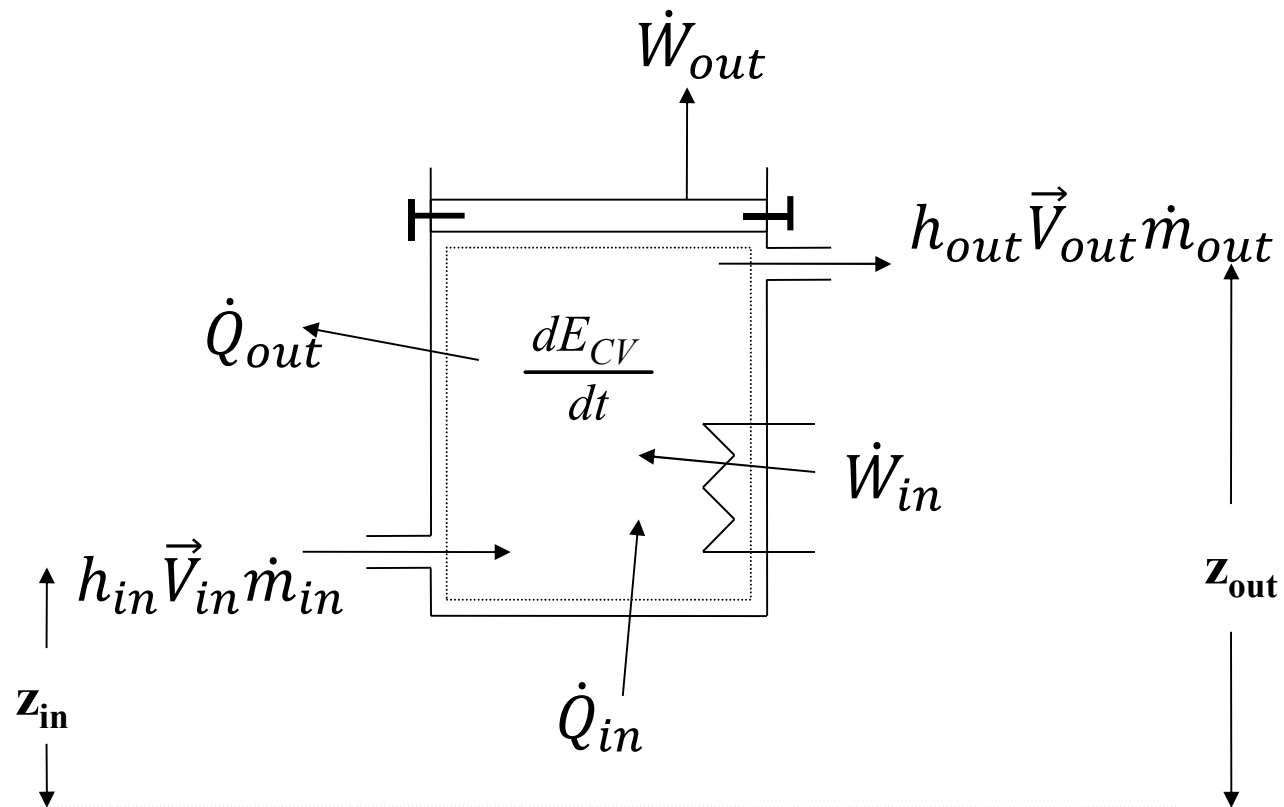


SSSF

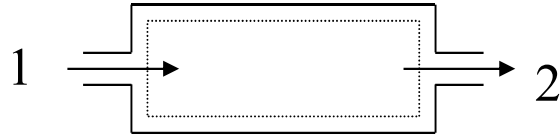
$$\dot{Q} - \dot{W} = \sum_{out} \dot{m} \left( h + \frac{\vec{V}^2}{2} + gz \right) - \sum_{in} \dot{m} \left( h + \frac{\vec{V}^2}{2} + gz \right)$$

For each **exit**  
channel

For each **inlet**  
channel



## SSSF energy equation for 1 inlet / 1 exit



**Mass**

$$\dot{m}_{in} = \dot{m}_{out} \quad \text{or} \quad \dot{m}_1 = \dot{m}_2$$

**Energy**

$$\dot{Q} - \dot{W} = \dot{m}_2 \left( h_2 + \frac{\vec{V}_2^2}{2} + gz_2 \right) - \dot{m}_1 \left( h_1 + \frac{\vec{V}_1^2}{2} + gz_1 \right)$$

$$\dot{m}_1 = \dot{m}_2 = \dot{m}$$

$$\dot{Q} - \dot{W} = \dot{m} \left[ (h_2 - h_1) + \left( \frac{\vec{V}_2^2}{2} - \frac{\vec{V}_1^2}{2} \right) + (gz_2 - gz_1) \right]$$

$$\frac{\dot{Q}}{\dot{m}} - \frac{\dot{W}}{\dot{m}} = (h_2 - h_1) + \left( \frac{\vec{V}_2^2}{2} - \frac{\vec{V}_1^2}{2} \right) + (gz_2 - gz_1)$$

$$q - w = \Delta h + \Delta ke + \Delta pe \quad (1 \text{ inlet} / 1 \text{ exit}) \quad (\Delta = \text{exit} - \text{inlet})$$

SSSF energy equation for multiple channels but neglecting  $\Delta ke$ ,  $\Delta pe$

$$\dot{Q} - \dot{W} = \sum \dot{m}_{out} h_{out} - \sum \dot{m}_{in} h_{in}$$

$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$

## SSSF Applications

For devices which are *open systems*

- (a) { Nozzle & Diffuser  
Turbine & compressor  
Throttling valve @ porous plug
- (b) { Mixing/Separation Chamber  
Heat exchanger(boiler, condenser, etc)

2 categories;

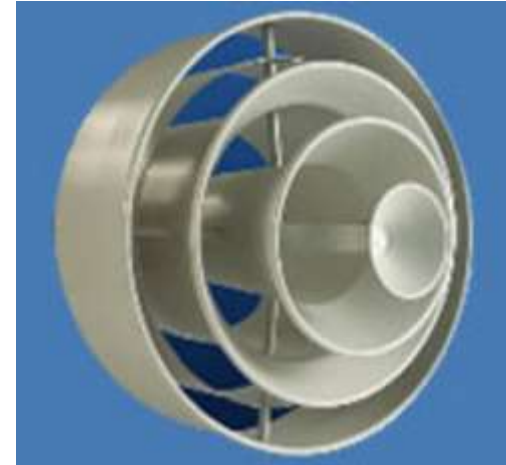
1 inlet / 1 outlet

Multiple inlet / outlet

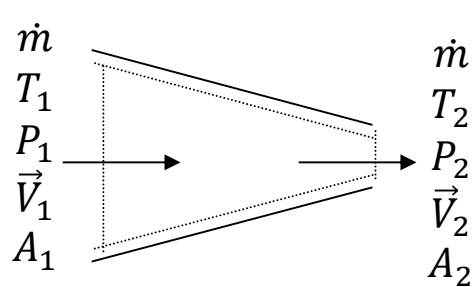
Analysis starts from the general SSSF energy equation;

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

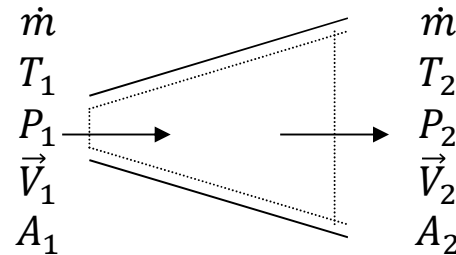
## Nozzle & Diffuser ( $\Delta KE \neq 0$ ) (To change fluid velocity)



## Nozzle & Diffuser ( $\Delta KE \neq 0$ ) (To change fluid velocity)



Nozzle     $\vec{V} \uparrow$



Diffuser     $\vec{V} \downarrow$

### Assumptions

Const. volume  $\rightarrow w_B = 0$   
 No other work

$$\left. \begin{array}{l} \text{Const. volume } \rightarrow w_B = 0 \\ \text{No other work} \end{array} \right\} w_{CV} = 0$$

Small difference in height  $\rightarrow \Delta pe = 0$

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

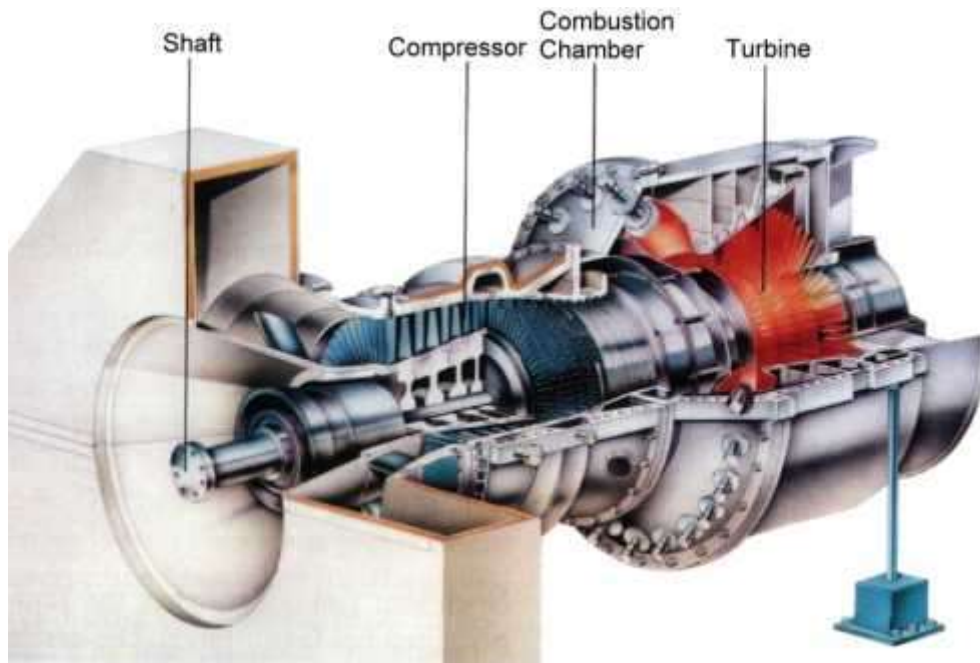
1 inlet / 1 outlet

$$q - \cancel{w} = \Delta h + \Delta ke + \cancel{\Delta pe}$$

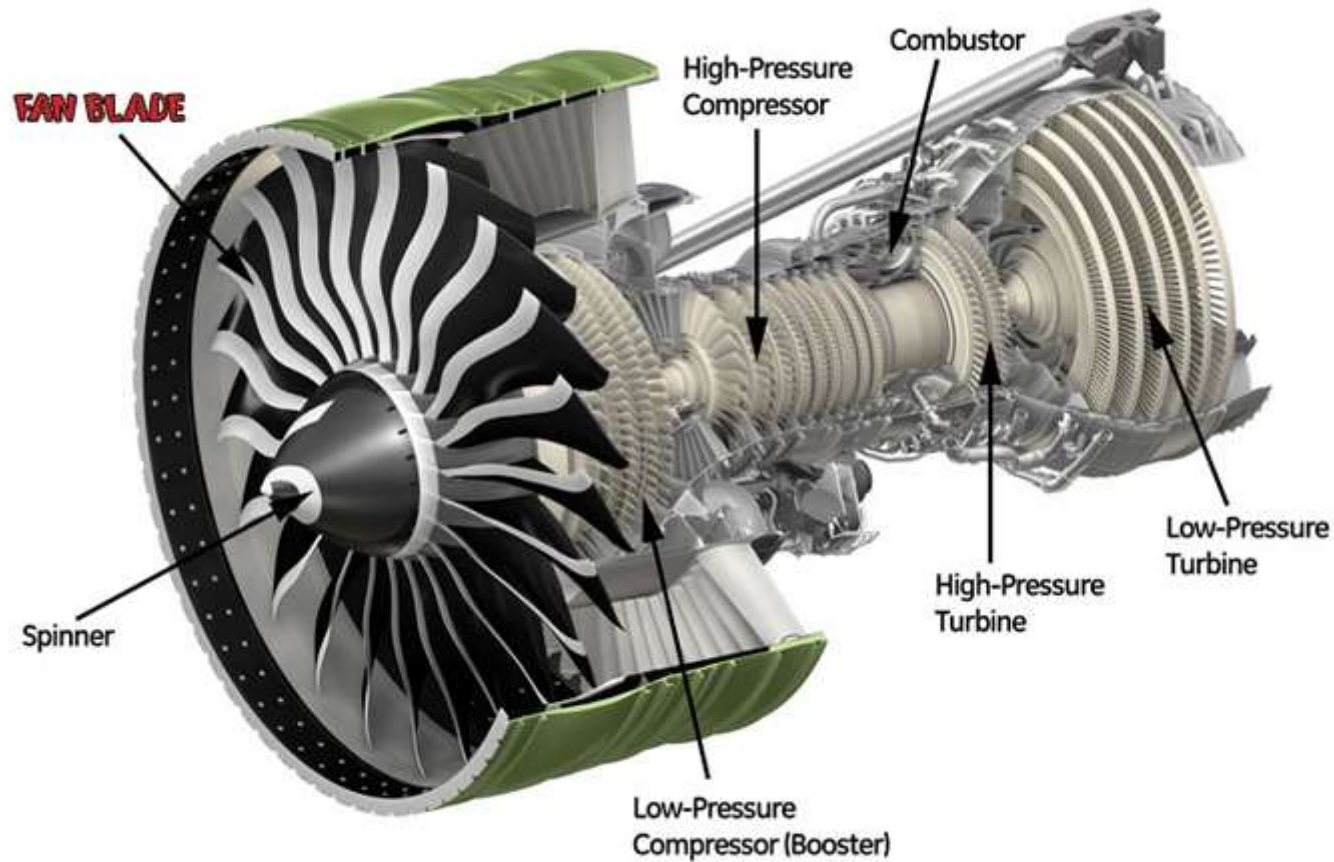
$$q = \Delta h + \Delta ke$$



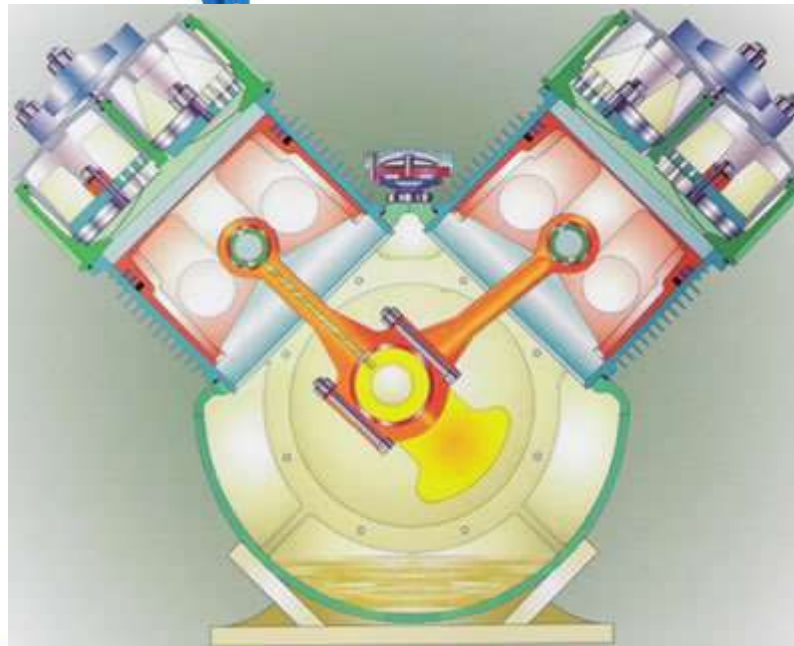
# Turbine ( $w_{CV} \neq 0$ )



# Turbine & Compressors ( $w_{CV} \neq 0$ )

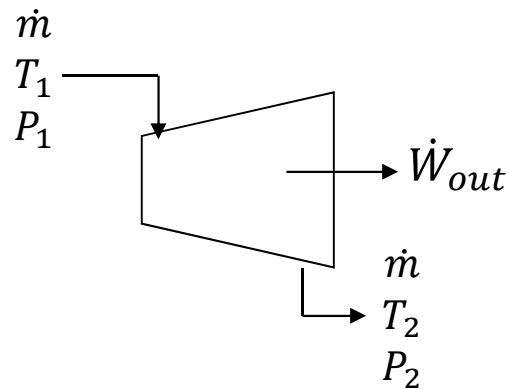


# Compressors (Reciprocating) ( $w_{CV} \neq 0$ )



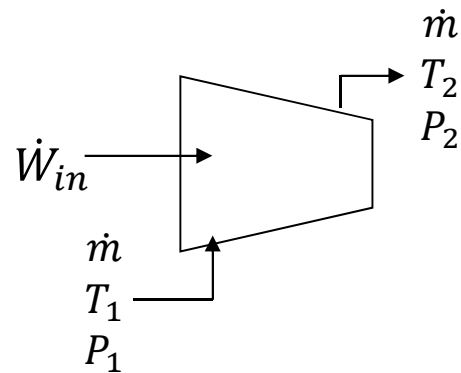
# Turbine & Compressor

$$(w_{CV} \neq 0)$$



## Turbine

produces work ( $W +ve$ )  
 from expansion of  
 fluid ( $\Delta P -ve$ )



## Compressor

increases pressure ( $\Delta P +ve$ )  
 using work supplied ( $W -ve$ )

## Assumptions

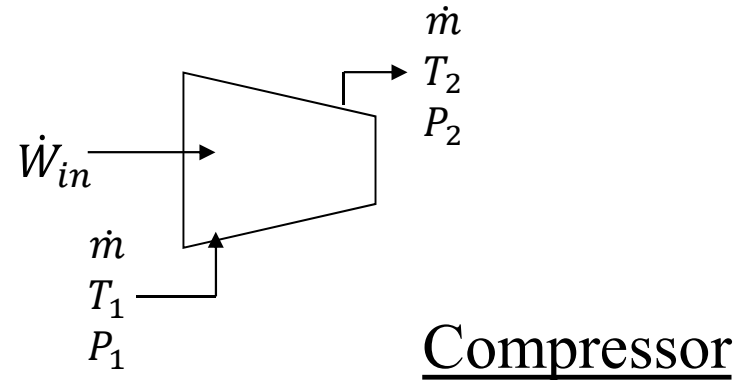
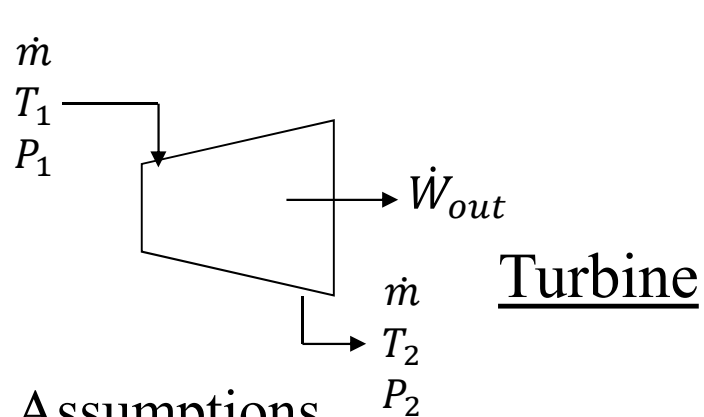
Const. volume  $\rightarrow w_B = 0$

Involves other work

Small difference in height  $\rightarrow \Delta p_e = 0$

$$\left. \begin{array}{l} \text{Const. volume} \rightarrow w_B = 0 \\ \text{Involves other work} \end{array} \right\} w_{CV} \neq 0$$

# Turbine & Compressor ( $w_{CV} \neq 0$ )



## Assumptions

Const. volume  $\rightarrow w_B = 0$   
 Involves other work  
 Small difference in height  $\rightarrow \Delta p_e = 0$

}  $w_{CV} \neq 0$

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

1 inlet / 1 outlet

$$\dot{Q} - \dot{W} = \dot{m}(\Delta h + \Delta ke + \cancel{\Delta pe})$$

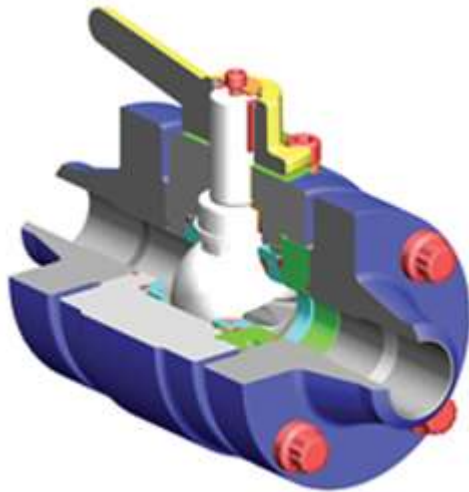
Commonly insulated ( $q=0$ ), and also  
 $\Delta ke \approx 0$  (since  $\Delta ke \ll \Delta h$ )

$$-\frac{\dot{W}}{\dot{m}} = \Delta h = h_2 - h_1$$

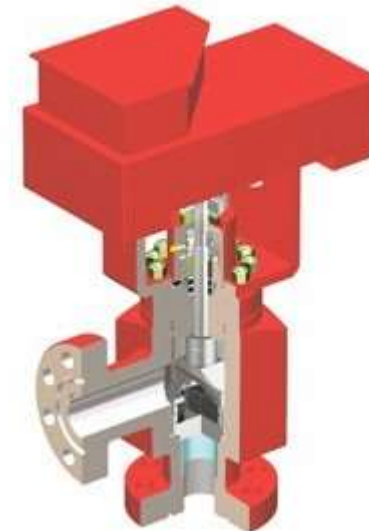
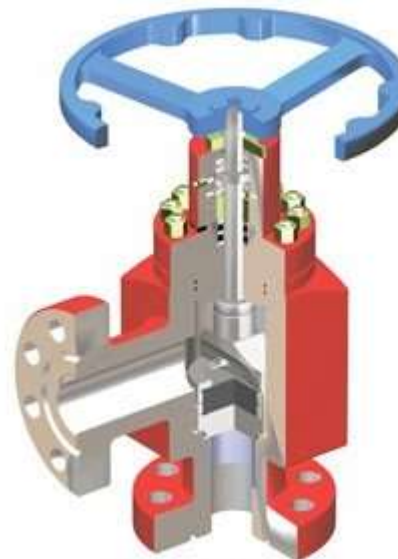


## Throttling valve/Porous plug (const. enthalpy, $h = c$ )

To reduce pressure without involving work



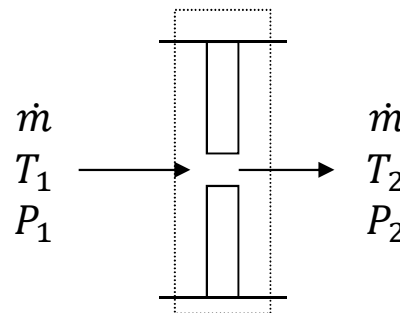
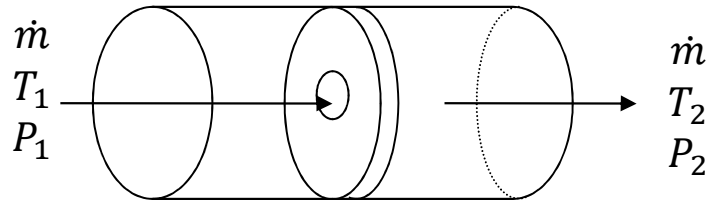
E-STORE





## Throttling valve/Porous plug (const. enthalpy, $h = c$ )

To reduce pressure without involving work



### Assumptions

$$W = 0$$

$$\Delta ke = 0, \Delta pe = 0$$

$$Q \approx 0 \text{ (system too small)}$$

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

1 inlet / 1 outlet

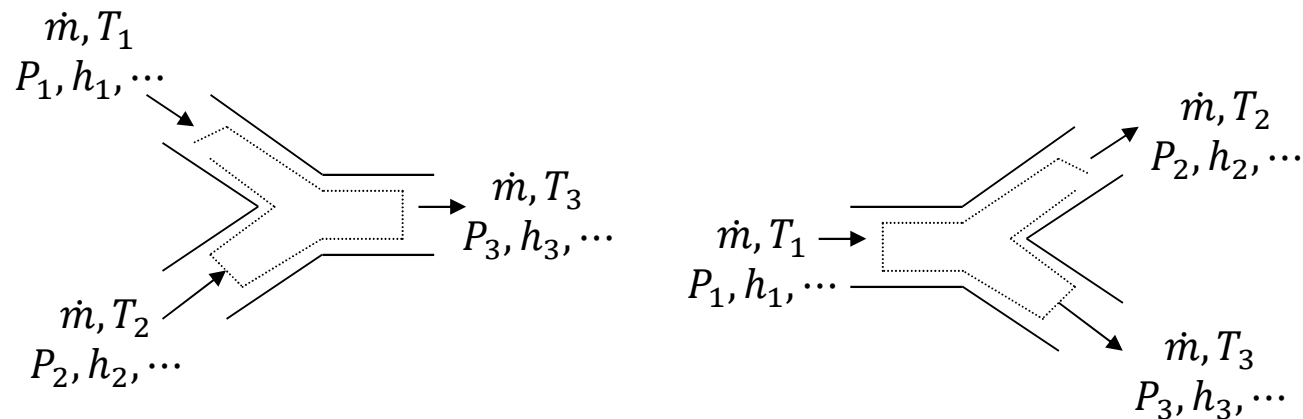
$$\cancel{\dot{Q}} - \cancel{\dot{W}} = \Delta h + \cancel{\Delta ke} + \cancel{\Delta pe}$$

$$\Delta h = 0$$

$$h_1 = h_2$$

For throttling valves

## Mixing/Separation Chamber / T junction pipe



### Assumptions

$$W_B = 0$$

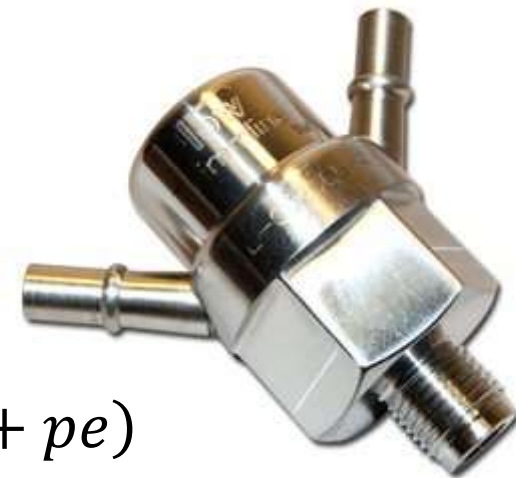
Same pressure at all channels

Other assumptions made accordingly

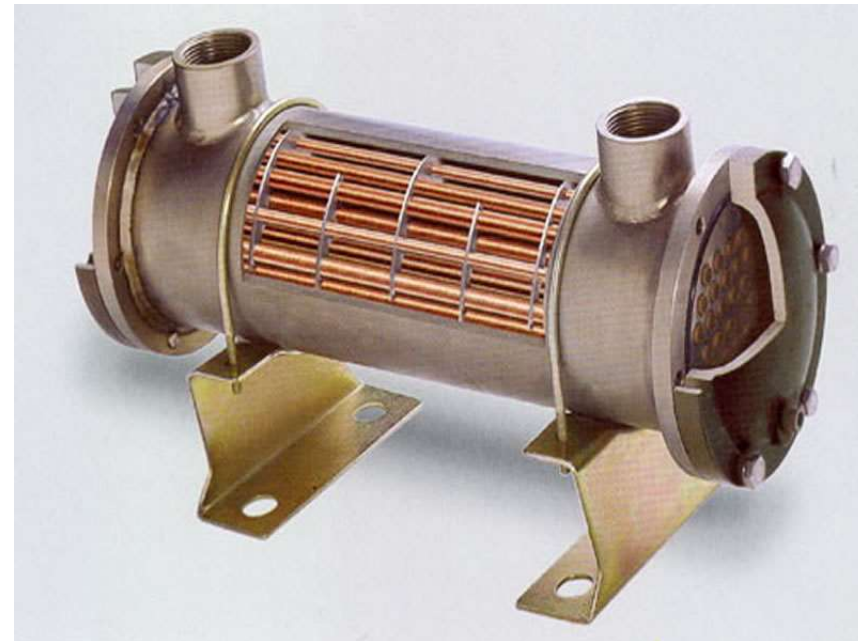
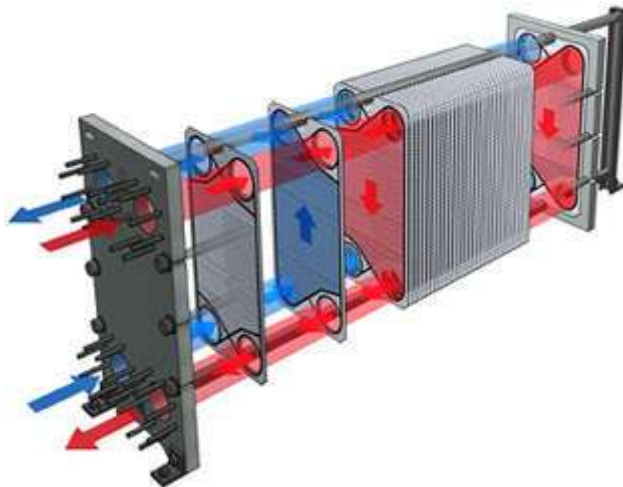
$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

also

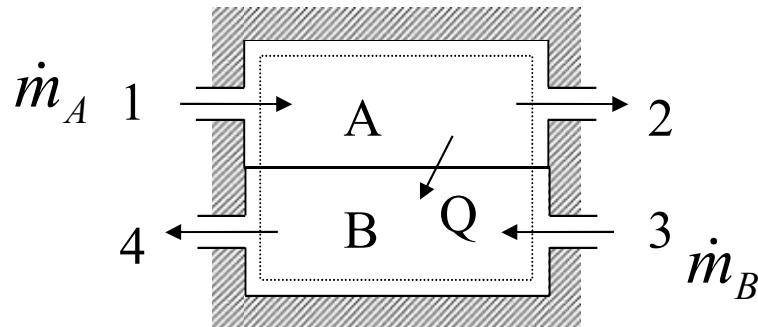
$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$



# Heat Exchangers



## Heat Exchangers



Assumptions (*System encompasses the whole heat exchanger*)

No work involved,  $W = 0$

Insulated,  $Q = 0$

$\Delta ke = 0$  ,  $\Delta pe = 0$

$$\cancel{\dot{Q}} - \cancel{\dot{W}} = \sum_{out} \dot{m}(h + \cancel{ke} + \cancel{pe}) - \sum_{in} \dot{m}(h + \cancel{ke} + \cancel{pe})$$

$$\sum \dot{m}_{in} h_{in} = \sum \dot{m}_{out} h_{out}$$

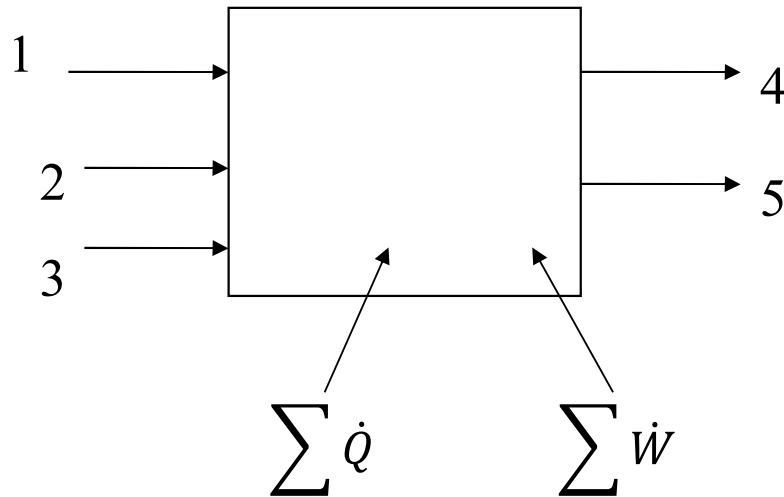
$$\dot{m}_A h_1 + \dot{m}_B h_3 = \dot{m}_A h_2 + \dot{m}_B h_4$$

$$\dot{m}_A (h_1 - h_2) = \dot{m}_B (h_4 - h_3)$$

also

$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$

## General device (Black box analysis)



Assumptions made according to situation...

$$\dot{Q} - \dot{W} = \sum_{out} \dot{m}(h + ke + pe) - \sum_{in} \dot{m}(h + ke + pe)$$

also 
$$\sum \dot{m}_{in} = \sum \dot{m}_{out}$$